

Grain growth in $\text{Na}_{0.5}\text{Bi}_{0.5}\text{TiO}_3$ -based solid solutions

L. Eglite^{a,b}, M. Antonova^a, E. Birks^a, M. Knite^b, and M. Livinsh^a

^aUniversity of Latvia, Institute of Solid State Physics, Riga, Latvia; ^bFaculty of Materials Science and Applied Chemistry, Institute of Technical Physics, Riga Technical University, Riga, Latvia

ABSTRACT

This paper discusses effects of different dopants, sintering technique and parameters on microstructure and properties of pure and Yb, Er-doped $\text{Na}_{0.5}\text{Bi}_{0.5}\text{TiO}_3$ (NBT). All stoichiometric compositions follow the abnormal grain growth mechanism (AGG) and exhibit a bimodal grain size distribution. Bi over-stoichiometry, two step sintering and hot pressing are effective inhibitors of AGG. Microstructure of sintered NBT greatly influences such properties as dielectric permittivity and depolarization temperature.

ARTICLE HISTORY

Received 
Accepted 

KEYWORDS

Lead-free ferroelectrics;
NBT; abnormal grain
growth; solid-state sintering

1. Introduction

Lead-free ferroelectric ceramic materials with a perovskite structure, including $\text{Na}_{0.5}\text{Bi}_{0.5}\text{TiO}_3$ (NBT), are often considered as promising candidates for substitution of traditional manufacturing materials containing lead, such as PZT and PMN-PT. NBT ceramics are characterized by their high coercive field of 73 kV/cm and low depolarization temperature of 187 °C [1, 2]. NBT is frequently modified to improve its properties, however the influence of grain growth and grain size distribution on physical properties is studied less frequently. In this context, sintering plays a vital part in microstructural evolution during which transformations in grain size distribution occur. In the case of NBT and NBT-based solid solutions, anomalous grain growth (AGG) is a common grain growth mechanism, wherein only a small fraction of grains grow rapidly and the microstructure is characterized by a bimodal grain size distribution. AGG is often undesirable because the heterogenous microstructure is not reproducible and can deteriorate physical properties, e.g. hardness, but can also improve other properties, such as fracture toughness [3].

Normal grain growth occurs in systems with rough (atomically disordered) grain boundaries and is controlled by diffusion, while abnormal grain growth occurs in systems with faceted (atomically ordered) grain boundaries and is controlled by interface reactions and diffusion. The microstructural evolution principle can be developed based on these considerations, where different types of grain coarsening behavior can occur because of the reciprocal relation between the maximum driving force for growth of the largest grain in a system (Δg_{max}) and the critical driving force for appreciable migration of the grain boundary (Δg_{c}). According to this principle, stagnant, abnormal, pseudo-normal and normal grain coarsening can take place with a reduction of Δg_{c} for a given Δg_{max} [4–6].

This study is focused on effects of doping, non-stoichiometry, sintering technique (conventional, two-step sintering and hot pressing) and parameters on the microstructure and properties of $\text{Na}_{0.5}\text{Bi}_{0.5}\text{TiO}_3$ and lanthanide (Yb, Er)-modified $\text{Na}_{0.5}\text{Bi}_{0.5}\text{TiO}_3$ compositions.

2. Experimental details

$\text{Na}_{0.5}\text{Bi}_{0.5}\text{TiO}_3$, $\text{Na}_{0.5}\text{Bi}_{0.52}\text{TiO}_3$, $\text{Na}_{0.5}\text{Bi}_{0.5}\text{Ln}_x\text{TiO}_3$ and $\text{Na}_{0.5}\text{Bi}_{0.52-x}\text{Ln}_x\text{TiO}_3$ (Ln = Yb, Er) ceramic samples were prepared through the conventional ceramic route using reagent grade oxide and carbonate powders of Na_2CO_3 , Bi_2O_3 , TiO_2 , Yb_2O_3 , Er_2O_3 (“Sigma-Aldrich”, “Acros Organics”). The raw materials were dried in an oven at 200°C for 4 hours to remove any adsorbed moisture. Dried raw powders were then weighed according to calculated compositions, mixed and ball-milled for 24 hours using ethanol (99.8%) as medium. The slurry was dried in an oven at 200°C for 4 hours. Powders were then crushed in a mortar and calcined in a corundum crucible at 850°C for 2 hours. Calcined powders were crushed in a pestle and the ball-milling, drying and crushing processes were repeated. Second calcination was carried out at $970\text{--}1000^\circ\text{C}$ for 2 hours. X-ray diffraction of the calcined powders showed that the calcined powders are of a single perovskite phase. The obtained powders were crushed in a pestle and mixed with a 3% polyvinyl alcohol (PVA) binder and pressed using a hydraulic hand press under 32 MPa (sample diameter $d = 17$ mm, height $h = 10$ mm).

Individual samples were hot-pressed at $1120\text{--}1180^\circ\text{C}$ for 2 hours, while the remaining samples were put in a corundum crucible, on a Pt plate, covered with a corundum lid, and conventionally sintered at $1170\text{--}1235^\circ\text{C}$ for 2–12 hours in air with a heating rate of $3\text{--}4^\circ\text{C}/\text{min}$. Some pressed pellets were two-step sintered, the process consisted of heating of the sample up to $1200\text{--}1250^\circ\text{C}$ followed by immediate cooling to $1100\text{--}1150^\circ\text{C}$ with a rate of $10^\circ\text{C}/\text{min}$ and holding at these temperatures for various times (10 min–12 hours). Crystallographic symmetry of dense ($\rho_{\text{relat.}} \geq 94\%$) $\text{Na}_{0.5}\text{Bi}_{0.5}\text{TiO}_3$ -based samples was analysed using X-ray powder diffraction with $\text{CuK}\alpha$ radiation (XRD, “PANalytical X’Pert PRO”) and exhibited a single perovskite phase. Microstructures were observed for polished and thermally etched ($1020\text{--}1135^\circ\text{C}$ for 3–4 h) samples using a scanning electron microscope (“Phenom Pro”). Linear intercept method was used to determine average grain size, statistical analysis of grain size distribution was conducted for 1000 grains of each composition. Chemical analysis was carried out using energy dispersive spectroscopy (“EDAX/Ametek Eagle III microprobe” and “Tescan MIRA/LMU” SEM equipped with “Oxford 7378” EDS spectroscope). Dielectric measurements were carried out using an impedance analyzer (“HP4284A”). Depolarization temperatures were determined from the frequency independent maximum of $\text{tg}\delta$ for previously poled samples.

3. Results and discussion

3.1. Changes in grain growth behaviour depending on the sintering parameters

Grain growth at various sintering times. Average grain size of $\text{Na}_{0.5}\text{Bi}_{0.5}\text{TiO}_3$ sintered at 1180°C has a tendency to decrease from $4.2 \pm 2.0 \mu\text{m}$ (at 10 min) to $3.5 \pm 1.8 \mu\text{m}$ (at 4 hours) upon increasing of sintering time at maximum temperature, while the fraction

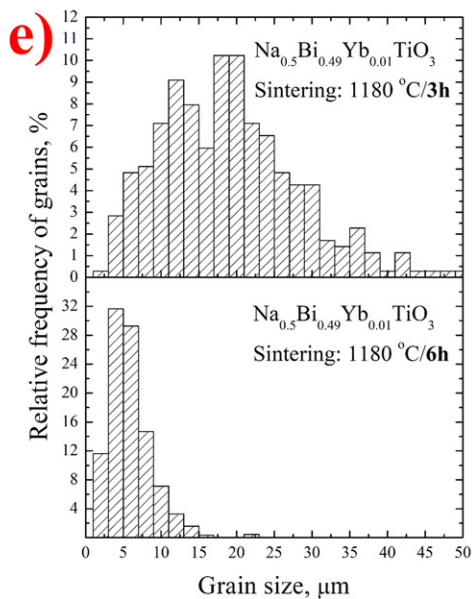
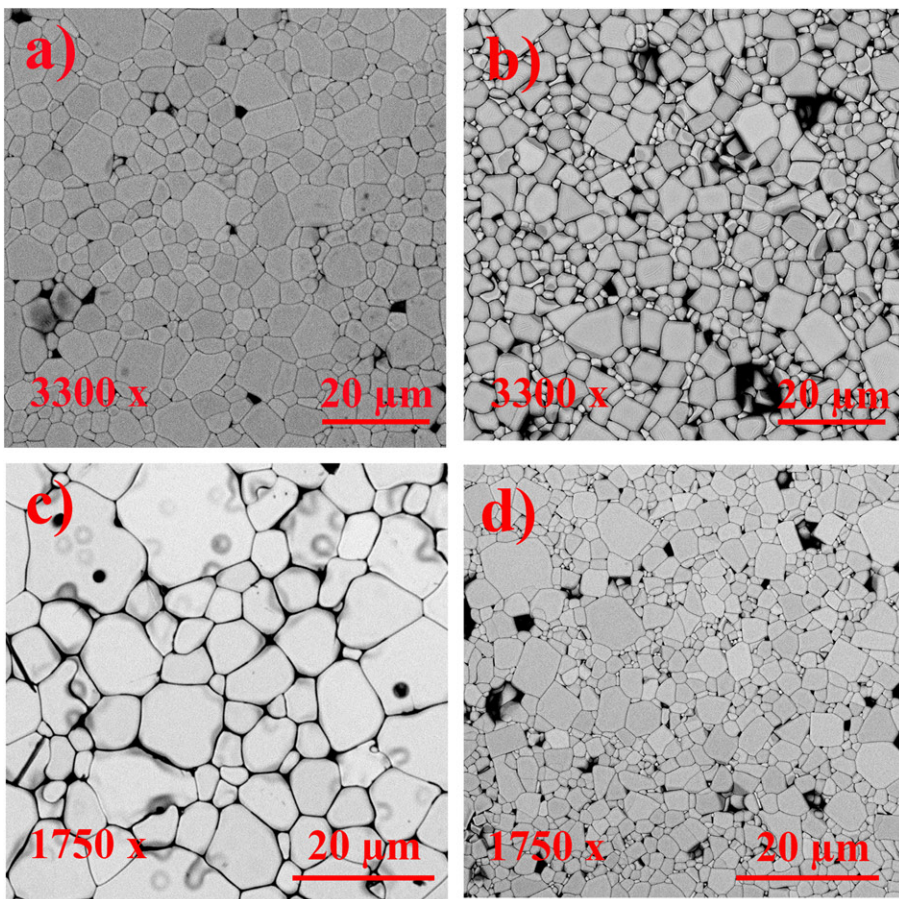


Figure 1. Micrographs of $\text{Na}_{0.5}\text{Bi}_{0.5}\text{TiO}_3$ sintered for a) 10 min; b) 4 h and of $\text{Na}_{0.5}\text{Bi}_{0.5}\text{Yb}_{0.01}\text{TiO}_3$ sintered for c) 3 hours; d) 6 hours and e) its grain size distribution

of faceted grains increases and bimodal grain size distribution becomes more pronounced (Figure 1a and b). Therefore, the critical driving force for appreciable grain boundary migration (Δg_c) increases as sintering time is increased. These are some of the key factors indicating AGG. The same correlation has also been identified in $\text{Na}_{0.5}\text{Bi}_{0.49}\text{Yb}_{0.01}\text{TiO}_3$, where grain size reduces from $18.0 \pm 9.2 \mu\text{m}$ (at 3 hours) to $4.9 \pm 2.9 \mu\text{m}$ (at 6 hours), grain size distribution becomes narrower and bimodality is more expressed (Figure 1c–e). A smaller fraction of abnormally large grains in a fine-grained matrix, observed at longer sintering times, does not outweigh the matrix of more uniformly distributed grains in terms of average grain size, therefore a reduction of average grain size with an increase in sintering time can be observed.

3.1.1. Grain growth at various sintering temperatures

Average grain size of A-site lanthanide substituted NBT, such as $\text{Na}_{0.5}\text{Bi}_{0.5-x}\text{Yb}_x\text{TiO}_3$ ($x = 0.005\text{--}0.05$), increases upon increasing of sintering temperature. In the case of $\text{Na}_{0.5}\text{Bi}_{0.49}\text{Yb}_{0.01}\text{TiO}_3$, as the sintering temperature is increased from 1170°C to 1180°C at a constant sintering time of 3 hours, grain size increases from $11.0 \pm 7.2 \mu\text{m}$ to $18.0 \pm 9.2 \mu\text{m}$ (Table 1). Grain boundaries are more faceted and grain size distribution is bimodal for samples sintered at 1170°C , whereas at 1180°C boundaries become rougher and the grain size distribution becomes more unimodal. This has been previously reported [6] – boundary structure is largely governed by the total vacancy concentration – faceted boundaries indicate a low vacancy concentration, whereas rough boundaries – high vacancy concentration. Evaporation of A-site ions, usually assumed to exist in NBT ceramics, induces a decrease in critical driving force Δg_c , leading to a transition from faceted to rough grain boundaries and inhibition of AGG. All stoichiometric $\text{Na}_{0.5}\text{Bi}_{0.5}\text{TiO}_3$ and lanthanide-doped $\text{Na}_{0.5}\text{Bi}_{0.5-x}\text{Ln}_x\text{TiO}_3$ ($\text{Ln} = \text{Yb}, \text{Er}$) compositions follow the AGG mechanism and exhibit a bimodal grain size distribution (Figure 1), independent of sintering time and temperature.

Energy dispersive spectroscopy (EDS) for A-site Er, Yb substituted NBT shows that as the intensity of ErL, YbL line increases, the bismuth line BiL decreases accordingly (Figure 2). This trend does not confirm previously considered presence of Bi vacancies (due to evaporation of Bi ions during sintering), because Er, Yb ions should occupy positions of Bi vacancies before they start replacing Bi therefore the content of Bi decreases. If A-site vacancies influence grain morphology, the average concentration of these vacancies should be vastly below 0.5 at.% [7].

Table 1. Average grain size in pure Er- and Yb-modified NBT compositions at different sintering temperatures.

$T_{\text{sintering}}, ^\circ\text{C}$	$t_{\text{sintering}}, \text{h}$	Composition	Average grain size, μm
1180	4	$\text{Na}_{0.5}\text{Bi}_{0.5}\text{TiO}_3$	3.6 ± 0.5
1170	3	$\text{Na}_{0.5}\text{Bi}_{0.49}\text{Yb}_{0.01}\text{TiO}_3$	11.0 ± 7.2
1180	3	$\text{Na}_{0.5}\text{Bi}_{0.49}\text{Yb}_{0.01}\text{TiO}_3$	18.0 ± 9.2
1180	3	$\text{Na}_{0.5}\text{Bi}_{0.51}\text{Yb}_{0.01}\text{TiO}_3$	3.0 ± 1.6
1180	4	$\text{Na}_{0.5}\text{Bi}_{0.492}\text{Er}_{0.008}\text{TiO}_3$	3.9 ± 0.6
1190	4	$\text{Na}_{0.5}\text{Bi}_{0.492}\text{Er}_{0.008}\text{TiO}_3$	4.2 ± 1.8
1180	4	$\text{Na}_{0.5}\text{Bi}_{0.512}\text{Er}_{0.008}\text{TiO}_3$	2.4 ± 1.2
1190	4	$\text{Na}_{0.5}\text{Bi}_{0.512}\text{Er}_{0.008}\text{TiO}_3$	3.2 ± 1.8

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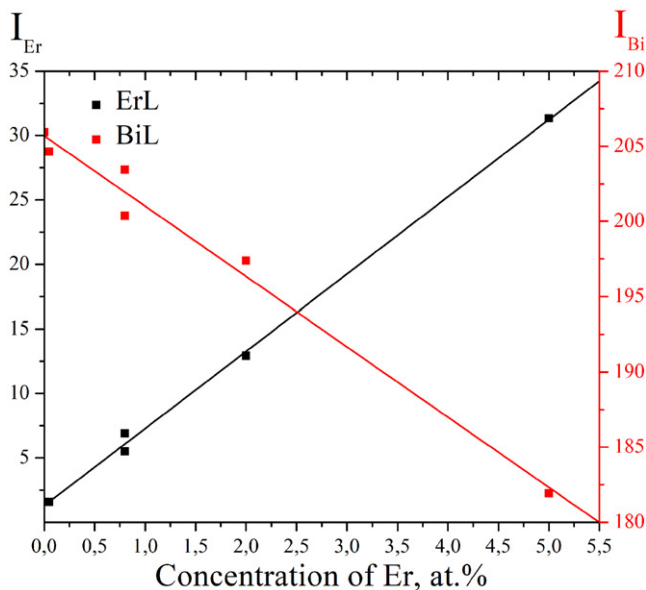


Figure 2. Bi and Er energy dispersive spectroscopy intensity dependence on concentration of erbium in $\text{Na}_{0.5}\text{Bi}_{0.5-x}\text{Er}_x\text{TiO}_3$ ($x = 0-0.05$) ceramics

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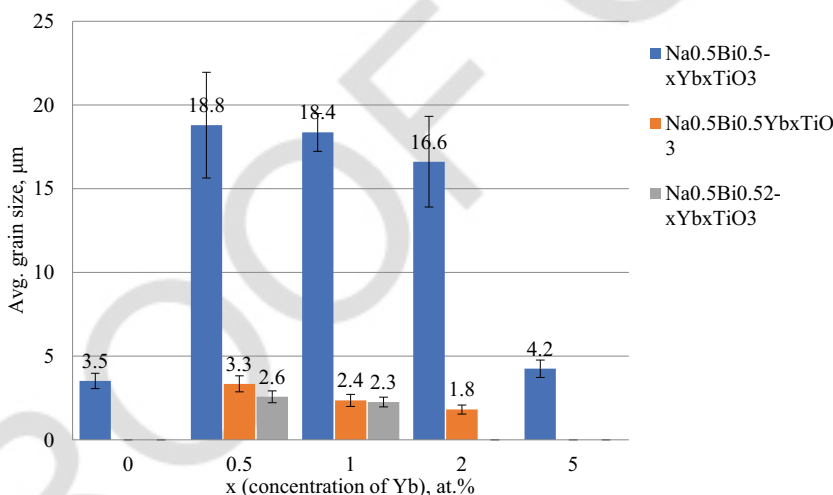


Figure 3. Average grain size of Yb-doped NBT ceramics

3.2. Grain growth behaviour in Bi-overstoichiometric samples

$\text{Na}_{0.5}\text{Bi}_{0.52}\text{TiO}_3$, $\text{Na}_{0.5}\text{Bi}_{0.52-x}\text{Yb}_x\text{TiO}_3$ and $\text{Na}_{0.5}\text{Bi}_{0.52-x}\text{Er}_x\text{TiO}_3$ over-stoichiometric compositions were sintered. Substantial reduction in average grain size in comparison with stoichiometric compositions is observed in all compositions (Figure 3). Apparently, over-stoichiometric amounts of Bi tend to decrease the energy required for grain growth. This can be attributed to the formation of a liquid phase in compositions with Bi over-stoichiometry. Nonetheless, these systems exhibit a bimodal grain size

distribution without the formation of abnormal grains. The larger grains are rough, while the smaller- faceted, therefore the presence of a liquid phase induces grain growth behaviour to change from abnormal to normal [8]. Bi-overstoichiometric samples also exhibit a correlation between concentrations of Bi and Er, Yb – the concentration of Bi decreases as concentration of Er, Yb increases.

3.3. Effect of two-step sintering and hot pressing

Two-step sintering was used for $\text{Na}_{0.5}\text{Bi}_{0.49}\text{Yb}_{0.01}\text{TiO}_3$ compositions, exhibiting larger grains compared to Er-containing compositions when sintered using the one-step conventional method. Sintering was carried out at two temperatures – after increasing the temperature up to 1200 °C, an immediate decrease to 1100 °C follows and this

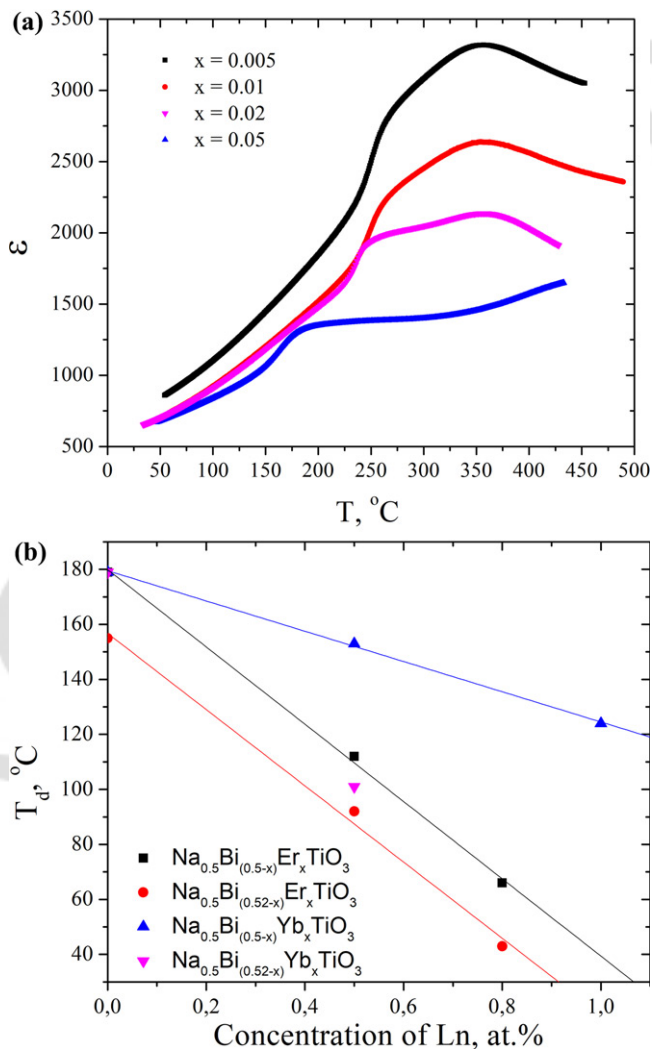


Figure 4. a) Dielectric permittivity dependence of temperature for $\text{Na}_{0.5}\text{Bi}_{0.5-x}\text{Yb}_x\text{TiO}_3$ at $f = 1$ kHz; b) depolarization temperature of Er, Yb-doped NBT as a function of concentration of Er/Yb

277 temperature is held constant for 10 min, 2 h, 6 h and 12 h. The minimum average grain
278 size of 1.49 μm was obtained for the shortest sintering time (10 min), while the largest
279 grain size of 2.4 μm – for 12 h sintering time at 1200 °C. Therefore, average grain size
280 increases as sintering time is increased which is contrary to conventional one-
281 step sintering.

282 Hot pressing was carried out at 1120 °C, 1170 °C and 1180 °C for 2 hours under the
283 force of 15 kN. An increase in sintering temperature leads to an increase in average
284 grain size and grain size distribution. In comparison with compositions sintered at
285 atmospheric pressure, hot pressed samples have a narrower grain size distribution and
286 average grain size (0.5 μm at $T_{\text{sintering}} = 1120$ °C). Therefore, hot pressing inhibits the
287 formation of abnormal grains and a wide grain size distribution.
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289 **3.4. Influence of microstructure on dielectric properties**

290 Addition of lanthanide dopants to NBT leads to a decrease in the maximum of tem-
291 perature dependence of dielectric permittivity and depolarization temperature
292 (Figure 4), thus reflecting a reduction of stability of the ferroelectric state. In Bi over-
293 stoichiometric compositions compared to stoichiometric compositions, depolarization
294 temperature decreases, most notably in Yb containing ones. The depolarization tem-
295 perature of $\text{Na}_{0.5}\text{Bi}_{0.5-x}\text{Yb}_x\text{TiO}_3$ is larger than in Bi over-stoichiometric, Er, Yb-contain-
296 ing compositions, which could be at least partly related to the larger grain size. Indeed,
297 stoichiometric $\text{Na}_{0.5}\text{Bi}_{0.49}\text{Yb}_{0.01}\text{TiO}_3$ compositions, sintered at different times exhibit a
298 reduction of T_d as the average grain size reduces.
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303 **4. Conclusions**

304 One-step conventionally sintered $\text{Na}_{0.5}\text{Bi}_{0.5-x}\text{Yb}_x\text{TiO}_3$ compositions exhibit a substantial
305 increase in average grain size at low concentrations of Yb ($x = 0.005\text{--}0.02$) and a pro-
306 nounced bimodal grain size distribution in comparison with NBT, which points to
307 AGG. For $\text{Na}_{0.5}\text{Bi}_{0.5-x}\text{Er}_x\text{TiO}_3$ the same mechanism applies, only the increase in average
308 grain size compared to NBT is insignificant. Bi over-stoichiometry for both Yb and Er-
309 modified NBT compositions lead to a reduction in average grain size and roughening of
310 grain boundaries, interpreted as the reduction of critical driving force Δg_c , therefore
311 inhibiting AGG. Bi over-stoichiometry may induce formation of a liquid phase that
312 increases the path of diffusion, therefore reducing the rate of grain growth.
313

314 Average grain size in one-step sintered samples tends to decrease and bimodality of
315 the grain size distribution becomes more pronounced with an increase in sintering
316 time, whereas in two-step sintered samples the opposite is true. Two-step sintering
317 tends to reduce broadening of the grain size distribution in comparison with one-step
318 sintering, especially at short sintering times. This method can be used to effectively sup-
319 press grain growth. Depolarization temperature in Er, Yb-doped NBT reduces along
320 with average grain size, which results in a reduction in stability of the ferroelectric state
321 within grains.
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